INTRODUCTION
Coherent detection with polarization division multiplexing (PDM) has emerged as the key technology enabler for 40 Gbps and 100 Gbps networks because it significantly increases the spectral efficiency of each channel and allows each channel to transmit at a high bit rate with relatively small optical bandwidth. Consequently, 40 Gbps, 100 Gbps, or even 160 Gbps channels can be transmitted over existing 10 Gbps WDM infrastructures with 50 GHz channel spacing [1]. PDM doubles the spectral efficiency by combining two polarization channels of the same bit rate at the same wavelength [2-8]. Also, coherent detection allows multiple levels of phase and amplitude modulation at lower rates to be multiplexed on the same wavelength channel [9-16]. For example, PDM, together with quadrature-phase-shift-keying (QPSK) modulation, enables 40 Gbps transmission within the bandwidth of a 10 Gbps direct channel [13]. At such a small bandwidth, impairments due to polarization mode dispersion (PMD) and chromatic dispersion (CD) are greatly reduced and have less impact on the bit error rate (BER) of the transmission. In addition, because both the amplitude and phase information of the two orthogonal polarizations of a signal are preserved in a coherent detection system, PMD, PDL (polarization dependent loss) and CD compensations can be performed by digital signal processing (DSP) in the electrical domain to further extend system tolerance of the effects of PMD, PDL, and CD.

A system deploying polarization multiplexing must be able to separate the two polarization channels at the receiving end. Such a task can be accomplished optically by controlling polarization with a feedback signal. Because both phase and amplitude information of both polarizations are maintained during coherent detection, the information can be obtained by digital signal processing (DSP). Digital polarization demultiplexing can significantly reduce cost and size, compared with optical demultiplexing.

POLARIZATION TEST REQUIREMENTS
Coherent detection systems generally perform the following polarization control functions:
- Polarization demultiplexing
- PMD compensation (PMDC)
- PDL compensation (PDLC)

These functions can be accomplished using high speed DSP circuits and algorithms in the transceivers. For transceiver developers, the evaluation of different DSP circuits and algorithms is critical. For the system integrators using the transceivers, it is important to compare the performance of transceivers from different vendors, including the three key polarization control functions. Finally, network operators using the systems developed by different system vendors can evaluate and compare the polarization performances from different vendors and optimize deployment decisions.

Polarization Demultiplexing Related Tests
For polarization demultiplexing, important testing parameters include:

- State of polarization (SOP) tracking speed
- SOP recovery time
- SOP orthogonality between the two polarization channels

SOP tracking speed is defined as the highest speed of SOP, measured in radians/second, at which a system can operate properly without losing track. It is a measure of how well the demultiplexing circuitry and algorithm track polarization variations of different patterns at different speeds.

SOP recovery time is defined as the time required for a system to recover from a loss of polarization track caused by an abrupt polarization change. It indicates how well the demultiplexing circuitry and algorithm respond to sudden SOP jumps.

Polarization orthogonality reflects the polarization channel crosstalk. In practice, it should be measured after two polarization channels are combined at the transmitter end and before they are separated at the receiving end. Ideally, the two polarization channels are perfectly orthogonal during transmission. However, imperfection in the polarization combiner can cause the two channels to be imperfectly orthogonal when they are combined. In addition, PMD, PDL, and nonlinearity may degrade the orthogonality of the two polarization channels and cause crosstalk. The degree of polarization (DOP) is an indication of polarization crosstalk. If there is no polarization crosstalk, the DOP is zero when the powers in the two polarization channels are equal. In the presence of crosstalk, the DOP is non-zero when the powers in the two polarization channels are equal.

PMD Related Tests
For PMD compensation, key performance indicators include SOP tracking speed, SOP recovery time, PMD tracking speed, PMD recovery time, and PMD tolerance range. Similar to their definitions in polarization demultiplexing, SOP tracking speed is defined as the highest polarization variation rate at which the PMD compensation (PMDC) hardware and algorithm can effectively reduce PMD related signal distortions, and SOP recovery time as the time required for a PMDC to recover from a loss of track caused by an abrupt polarization jump.

PMD tracking speed is defined as the highest PMD variation speed at which the PMD compensator is still effective in reducing PMD induced signal distortion. It is specified in picoseconds/second and defines how fast a PMDC can respond to PMD value changes.

PMD recovery time is defined as the time required for a PMDC to recover from a loss of track caused by an abrupt PMD value jump. It measures how well a PMDC responds to sudden changes in PMD.

PMD tolerance range is defined as the maximum PMD value in a transmission system with which data can be transmitted with a BER smaller than that required by system design. It is a measure of how well the PMDC works in mitigating PMD effects and extending the system’s PMD tolerance range.

PDL Related Tests
For PDL testing, the critical parameters are SOP tracking speed, SOP recovery time, PDL tracking speed, PDL recovery time,
and PDL tolerance range. SOP tracking speed is defined as the highest SOP variation speed at which the PDLC can still function effectively in reducing PDL related transmission errors. SOP recovery time is defined as the time required for a PDLC to recover from a loss of track caused by an abrupt polarization change. PDL tracking speed is defined as the highest rate of PDL change (in units of dB/s) at which a PDLC can effectively reduce PDL related errors. PDL recovery time is defined as the time required for a PDLC to recover from a loss of track caused by an abrupt PDL change. Finally, PDL tolerance range is the maximum PDL value in a transmission system with which data can be transmitted with an acceptable BER. It is a measure of how well a PDLC works in mitigating PDL effects and in extending the system’s PDL tolerance range.

Table I (below) summarizes the tests required for each function of a coherent detection system.

<table>
<thead>
<tr>
<th>Function</th>
<th>Polarization Demux</th>
<th>PMDC</th>
<th>PDLC</th>
</tr>
</thead>
<tbody>
<tr>
<td>SOP Tracking Speed</td>
<td>SOP Tracking Speed</td>
<td>SOP Tracking Speed</td>
<td>SOP Tracking Speed</td>
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<tr>
<td>SOP Recovery Time</td>
<td>SOP Recovery Time</td>
<td>SOP Recovery Time</td>
<td>PDLC Tracking Speed</td>
</tr>
<tr>
<td>SOP Orthogonality</td>
<td>PMD Tracking Speed</td>
<td>PMD Recovery Time</td>
<td>PDL Recovery Time</td>
</tr>
<tr>
<td></td>
<td>PMD Tolerance Range</td>
<td></td>
<td>PDL Tolerance Range</td>
</tr>
</tbody>
</table>

This scrambling method is therefore uniquely suited to SOP tracking speed testing.

![Fig. 3a) Tornado SOP trace, fixed axis. b) Tornado SOP trace, rotating axis. c) Tornado scrambling SOP rate variation distribution.](image)

2. Polarization Variation Emulation

SOP changes continuously in real fiber, as shown in Fig. 3d, with a variation rate that follows a Rayleigh distribution, as shown in Fig. 3e. The MPC-202 can generate this polarization variation pattern, with a mean rate of polarization variation that can be selected within a range of 0.01 to 2000 rad/s. This function can be used to model the effect of SOP variation in a real fiber system.

![Fig. 3d) SOP trace generated by the Rayleigh scrambling function.](image)

3. Abrupt, Random Polarization Change

The SOP changes between discrete points distributed uniformly across the Poincare Sphere, at a rate of change ranging from 0.01 to 20000 points/s.
However, because the Agilent 11896A was the first mainstream polarization controller available, many engineers are familiar with and rely on its polarization scrambling characteristics. For compatibility with this early standard, the MPC-202 has an Agilent 11896A emulation function that replicates the scrambling function of the Agilent polarization controller.

Polarization Orthogonality Test
The SOPs of the two polarization channels should ideally be orthogonal in the transmission fiber from the time that they are combined (or multiplexed) by a polarization beam combiner (PBC) at the transmission side until they are separated (or demultiplexed) by a polarization beam splitter (PBS) at the receiving end. Imperfections in PBCs can cause non-orthogonality, and standard specifications, such as polarization extinction ratio (PER), do not always properly reflect the orthogonality performance of the PBC; special tests are therefore required.

Two General Photonics instruments can be used for testing the orthogonality of a PBC: the POD-201 in-line polarimeter and the PSGA-101A polarization measurement system (Figure 4).

Polarization orthogonality may also degrade during transmission due to the effects of PMD, PDL, or nonlinearity. Again, both the POD-201 and PSGA-101 can be used to quantify the degradation by using the measurement method described above before the PBS at the receiver side.
PMD Tracking Speed and PMD Recovery Time Tests

For PMDC using DSPs in a coherent system, the circuit/algorithm must track SOP variations and rapid PMD changes. In order to test a PMDC’s PMD variation tracking speed and PMD recovery time, an instrument with fast PMD generation capability is required. The General Photonics PMDPro™ is recommended for these tests.

The PMDPro™ consists of a polarization controller, a front polarimeter, a PMD generator, and a rear polarimeter (Figure 5). The polarization controller can be used with the front polarimeter to automatically align and maintain the input SOP at 45° from the principal axis of the DGD element to obtain the worst-case first-order PMD effect. Alternatively, the controller can automatically adjust and maintain the input SOP using the feedback from the rear polarimeter to either minimize or maximize the output DOP for each PMD setting. Minimizing the output DOP enables testing of the worst-case total PMD effect, while maximizing the DOP turns the PMDPro™ into a PMD compensator, allowing the user to measure the PMD values of an active fiber link.

The PMDPro™ can also perform PMD emulation by generating statistical PMD distributions. Finally, the polarization controller and polarimeters can provide various polarization control functions, including variable rate polarization scrambling, polarization waveform generation, polarization trace generation and polarization stabilization at any SOP.

The PMD generator inside the PMDPro™ can deterministically generate both 1st and 2nd order PMD (SOPMD) values in a few milliseconds because the all digital design utilizes no mechanical rotators. Figure 6 shows available values of DGD and SOPMD.

Different operation modes provide different PMD change patterns for the two different tests: For PMD recovery time testing, the discrete PMD generation mode allows the user to change PMD values discontinuously with user selected step sizes and dwell times. The abrupt PMD jump offered in this mode will cause loss of track in the PMDC and enable the user to measure the time required for the PMDC to regain track. For PMD tracking speed testing, the continuous PMD generation mode allows the user to vary PMD values along a trace like those shown in the second graph in Fig. 6. Operators can gradually increase the PMD variation speed until the PMDC can no longer follow.

PMD Tolerance Test

Coherent Detection systems use DSP to increase PMD tolerance. PMD tolerance tests measure the maximum PMD value that the system can tolerate. A typical test setup is shown in Fig. 7a.

Test results can be used by network operators to compare systems made by different vendors and verify PMD related specifications promised by the vendors. They can also be used by system vendors to determine suitability of PMD algorithms, to tune algorithms, and for quality control screening of the transceivers. The key instrument in this setup is the PMD source used to generate precise 1st and 2nd order PMD values, as shown in Fig. 7a. The bit-error rate (BER) of the system, or another performance indicator parameter such as power penalty, is monitored as the 1st order PMD (DGD) values generated by the PMD source are increased until the BER reaches the limits of the system, as shown in Fig. 7b. The corresponding DGD is the 1st order PMD tolerance of the system. Both the 1st and 2nd order PMD (SOPMD) values can also be increased as the BER of the system is measured and plotted, as shown in Fig. 7c. The system outage probability can be calculated from the data obtained.

The effect of PMD on a system is highly dependent on the input SOP. To eliminate test uncertainties and increase test speed, the input SOP must be optimized and maintained against polarization fluctuations caused by external disturbances. For a single polarization system without multiplexing, the PMDPro™ has two modes of polarization optimization for PMD tolerance tests. One mode aligns the input SOP 45 degrees from the principal axes of the DGD generator to obtain the worst-case DGD effect. The second mode aligns the SOP by minimizing the output DOP to obtain the worst-case total PMD effect on the signal. Polarization optimization assures consistent and repeatable PMD tolerance test results.

In polarization multiplexed systems, where two orthogonal
polarization channels are present simultaneously, the PMDPro™'s polarization optimization functions are not useful; however, the built-in polarization scrambling functions can be used to scan through all possible polarization states to assure that the worst-case polarization effects are properly characterized.

Polarization Dependent Loss (PDL) Tolerance Test

A coherent detection system generally includes hardware and algorithms to compensate for the effects of PDL (PDLC). System vendors and operators need to know how much PDL a transceiver can tolerate, and therefore must conduct tolerance range testing. A system vendor can use test results to optimize hardware and algorithms, and to perform quality checks. Network operators can use PDL tolerance range testing to qualify vendors and to perform quality inspection of incoming equipment to ensure the performance of their systems.

Component Level PMD/PDL Measurements

The General Photonics PSGA-101A is recommended for characterization of PMD and PDL for component testing [17]. As shown in Fig. 9a, the PDL emulator generates any PDL value from 0 dB to 20 dB with a speed of less than 5 ms and a resolution of 0.1 dB. The PDL value can be set individually or can be scanned with a user defined range, waveform, and speed. In addition, random PDL variations can be generated to emulate PDL variations in a real system.

PDL Tracking Speed and Recovery Time Tests

PDL changes rapidly with time in real systems. It is therefore important to evaluate whether the PDL compensation can track the PDL changes. In order to test the PDL tracking speed of the PDL compensation, an instrument to generate fast PDL variations is essential. The PDLE-101’s ability to generate PDL changes using different wave forms is uniquely suited to such an application. Fig. 9b shows such a PDL variation following a triangle wave modulation.

The PDLE-101 can also generate abrupt PDL jumps in the form of a square wave, as shown in Fig. 9c. The abrupt PDL jump can cause the PDLC to lose track of the PDL, enabling the measurement of the time required for the PDLC to regain track for PDL compensation.

![Fig. 9b) Triangle wave PDL variation](image)

![Fig. 9c) Random amplitude square wave PDL variation](image)

General Photonics’ PDL emulator, the PDLE-101, is designed for PDL related system tests, particularly PDL tolerance testing. The emulator can set any PDL value from 0 dB to 20 dB with a speed of less than 5 ms and a resolution of 0.1 dB. The PDL value can be set individually or can be scanned with a user defined range, waveform, and speed. In addition, random PDL variations can be generated to emulate PDL variations in a real system.

**Table of Measurement Accuracy**

<table>
<thead>
<tr>
<th></th>
<th>DGD (1st Order PMD)</th>
<th>SOPMD (2nd Order PMD)</th>
<th>PDL</th>
</tr>
</thead>
<tbody>
<tr>
<td>Accuracy</td>
<td>± 2.6 femtoseconds</td>
<td>± 1.39 ps²</td>
<td>± 0.06 dB</td>
</tr>
<tr>
<td>Resolution</td>
<td>1 femtosecond</td>
<td>0.005 ps²</td>
<td>0.01 dB</td>
</tr>
<tr>
<td>Repeatability</td>
<td>0.022 femtoseconds</td>
<td>0.28 ps²</td>
<td>0.034 dB</td>
</tr>
</tbody>
</table>

General Photonics Corporation 909.590.5473  www.generalphotonics.com
In-Circuit Link PMD Measurement

It is often desirable to be able to measure the PMD of a transmission link without interrupting signal transmission. The General Photonics PMDPro™ has an in-service PMD measurement function, which is accomplished by PMD compensation, as shown in Fig. 11. On the Tx side, a polarized broadband light source, centered on an ITU grid with a 3-dB bandwidth of 0.25 nm and obtained by passing an ASE source through a tunable filter, is fed into an idle channel at the multiplexer. On the Rx side, the test signal is dropped out from the demultiplexing port and passes through a PMDPro™. The instrument generates DGD values between 0 and 90 ps with an incremental step of 0.357 ps. The time required to run one step is less than 1 ms. At any DGD value, PMD compensation can be performed by feeding the DOP value to the DSP circuit for it to control the polarization controller to maximize the DOP. To measure the PMD of the light path, the DGD value generated by the compensator steps from zero to its maximum value, while PMD compensation is performed by maximizing the DOP for each step. When the test signal reaches its peak DOP value, as shown in Fig. 11b, the DGD value of the compensator at this point is equal to the PMD value of the light path.

![Diagram](image)

General Photonics engineers demonstrated this in-service PMD characterization in a traffic carrying long haul network at a Verizon facility. The expected mean DGD of the route was calculated from the mean DGD values of the individual fiber sections using commercially available PMD measurement equipment before the long-haul system was installed and, before traffic commenced. The calculated value was 19.77 ps. The length of the route is 414 kilometers with a ROADM at each end. In the trial, the PMD values of 16 idle channels were measured. Figure 11c shows the measured DGD values of the 16 channels with error bars. The DGD value averaged over all 16 channels is 18.57 ps, which is very close to the expected mean DGD value of 19.77 ps. Considering the limited number of data points (channel numbers), the 6% difference between this result and the aforementioned “expected mean DGD” falls within the fundamental Gisin uncertainty [10].

The insert of Fig. 11c shows the results of a long-term PMD measurement of a single DWDM channel at 195.7 Thz. Fairly stable PMD values for the channel were observed during the measurement period, taken around midnight. Note that the time average of single channel PMD for a much longer time can also yield the average PMD of the fiber link. The trial results show that the instrument is sufficiently accurate in PMD measurement, and that the measurement has no impact on the live traffic of other signal carrying channels.

We also successfully demonstrated the PMDPro™'s PMD measurement by PMD compensation function at Verizon's 1500 km test bed using a 40Gbps signal itself as the signal source for the test with a DWDM channel for about 12 hours. The average PMD result obtained was very close to the expected value of the link. This result verified the usefulness of the PMDPro™ for the monitoring of the PMD of a fiber link over an in-use DWDM channel.

Summary

Coherent detection systems for 40Gbps and 100Gbps use digital signal processing for polarization demultiplexing, PMD compensation, and PDL mitigation. To quantify the performance of those functions, multiple tests are required. The first column of Table II (below) lists some polarization related tests of coherent detection systems. General Photonics provides an array
of instruments, listed in the first row of Table II, to facilitate those tests. The applicability of each instrument to particular tests are checked in the table.

<table>
<thead>
<tr>
<th>Instrument Description</th>
<th>SOP Tracking Speed Test</th>
<th>SOP Recovery Time Test</th>
<th>SOP Orthogonality</th>
<th>SOP &amp; DOP Viewing and Monitoring</th>
<th>PMD Tracking Speed Test</th>
<th>PMD Recovery Time Test</th>
<th>PMD Tolerance Range Test</th>
<th>PDL Tracking Speed Test</th>
<th>PDL Recovery Time Test</th>
<th>PDL Tolerance Range Test</th>
<th>PMD/PDL Measurement</th>
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<tr>
<td>Multifunction Polarization controller MPC-202</td>
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<td>Polarization measurement system PSGA-101A</td>
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</table>

References

[12] Y. Cai, OFC'2008, paper OTuM1